

22NRM06 ADMIT

Characterisation of AC and DC MV instrument transformers in extended frequency range up to 150 kHz

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WP1 - Performance requirements, parameters and test procedures for accuracy evaluation

Mario Luiso, Università degli Studi della Campania «Luigi Vanvitelli»

22NRM06 ADMIT - Second Stakeholder Workshop

Virtual, 16 January 2025



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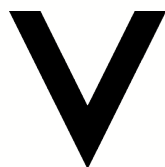
Dipartimento di Ingegneria

Acknowledgement

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ADMIT WP1 Status of activities
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2nd Workshop - 16th January 2025

Content

- Review of literature and standards for Power Grids and Instrument Transformers up to 150 kHz
- High Frequency Distortion (supraharmonics) effects
- Measurement campaign
- Laboratory test setup and VT testing results

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Scientific literature



Scientific Literature review

- Typical amplitudes and frequencies of High Frequency Distortions (HFDs)
- Measurement methods for HFDs
- Propagation of HFDs
- Mitigation strategies for HFDs

Typical amplitudes and frequencies of HFDs

- **Sources:** Mainly PhotoVoltaic (PV) power parks and Electric Vehicle (EV) Chargers (EVC). Their emissions are mainly concentrated in the range 2-50 kHz
- **Typical switching frequencies:** 10, 16, 45 kHz
- **Typical HFD Frequencies:**
 - PV: 10, 16, 26, 36, 126 kHz
 - EVC: 16, 32, 45, 48, 90 kHz
 - Intermodulation between PV and EVC: 16, 32, 48, 52, 64, 68, 80, 84, 96, 100 kHz
- **Typical HFD Amplitudes:** < 0.1 % for voltage, < 0.25 % for current
- **Typical transfer ratios:**
 - LV -> MV: 1 A/A, 0.01 to 1.0 V/V
 - MV -> LV: 0.5 to 3.0 V/V

Measurement methods for HFDs

- **Standard Measurement Techniques:** IEC 61000-4-7, IEC 61000-4-30, and CISPR 16-1
- **Other techniques:**
 - **Time-domain** methods include Digital CISPR, Light-QP, Numerical Heterodyne, matrix pencil method. They offer high time resolution, reduction of coloured noise but limitations on computational complexity and lower accuracy for high-amplitude components
 - **Frequency-domain** methods are based on Fourier Transform; they provide detailed frequency resolution but require higher sampling rates
- **Challenges:** Measurement devices may struggle with low-amplitude HFDs, leading to reduced accuracy, especially when the amplitude is below 5% of the fundamental frequency
- Analyzed literature do not consider the influence of Instrument Transformers on HFD measurements

Propagation of HFDs

- **Grid Impedance:** HFD propagation depends on the impedance of both low-voltage (LV) and medium-voltage (MV) grids. Propagation is simplified by the resonances, present both in AC as well as in DC grids
- **Propagation Mechanism:** HFDs can propagate from MV to LV grids and vice versa, especially through transformers, affecting the connected devices at both sides

Mitigation strategies for HFDs

- **Filters:** Various filters, including EMC filters, passive filters, and active filters, are employed to reduce HFDs by providing low-impedance paths for high-frequency signals
- **Resonance and Impedance Control:** Managing resonance and grid impedance can help to mitigate the propagation of HFDs
- **Challenges in Mitigation:** The propagation of HFDs through transformers complicates the mitigation process. Additionally, interference with power delivery equipment and end-user devices can complicate identifying the source of disturbances.

Standard review



International standards for HFDs

There is not a specific standard that cover disturbances in the range 9-150 kHz

1. Voltage Characteristics of Electricity Supplied by Public Distribution Networks

- **EN 50160**: Defines voltage characteristics for public electricity distribution systems
- **IEC 62749**: Relates to power quality in the grid.

2. Recommended Practice for Monitoring Electric Power Quality

- **IEEE 1159**: Provides guidelines for monitoring and analyzing power quality, including HFDs.

3. Electromagnetic Compatibility (EMC)

- **IEC 61000**: Specifies immunity and emission requirements for electrical and electronic equipment in the context of EMC.

4. Instrument Transformers (ITs)

- **IEC 61869**: Standards related to current and voltage transformers, crucial for accurately measuring HFDs in MV grids.



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Overview of supraharmonics negative effects



Power losses in conductors, such as skin effects and proximity effects



Aging of insulating materials and capacitors



Damage to MV cable terminations caused by local heating and electric field gradient;



Overview of supraharmonics negative effects



Triggering of network resonances



Interference with equipment connected at the LV level (domestic appliances, information technology (IT), lighting, energy meters, etc...)



Flicker phenomena on LED and fluorescent lamps



Specific interference with power line communication (PLC)

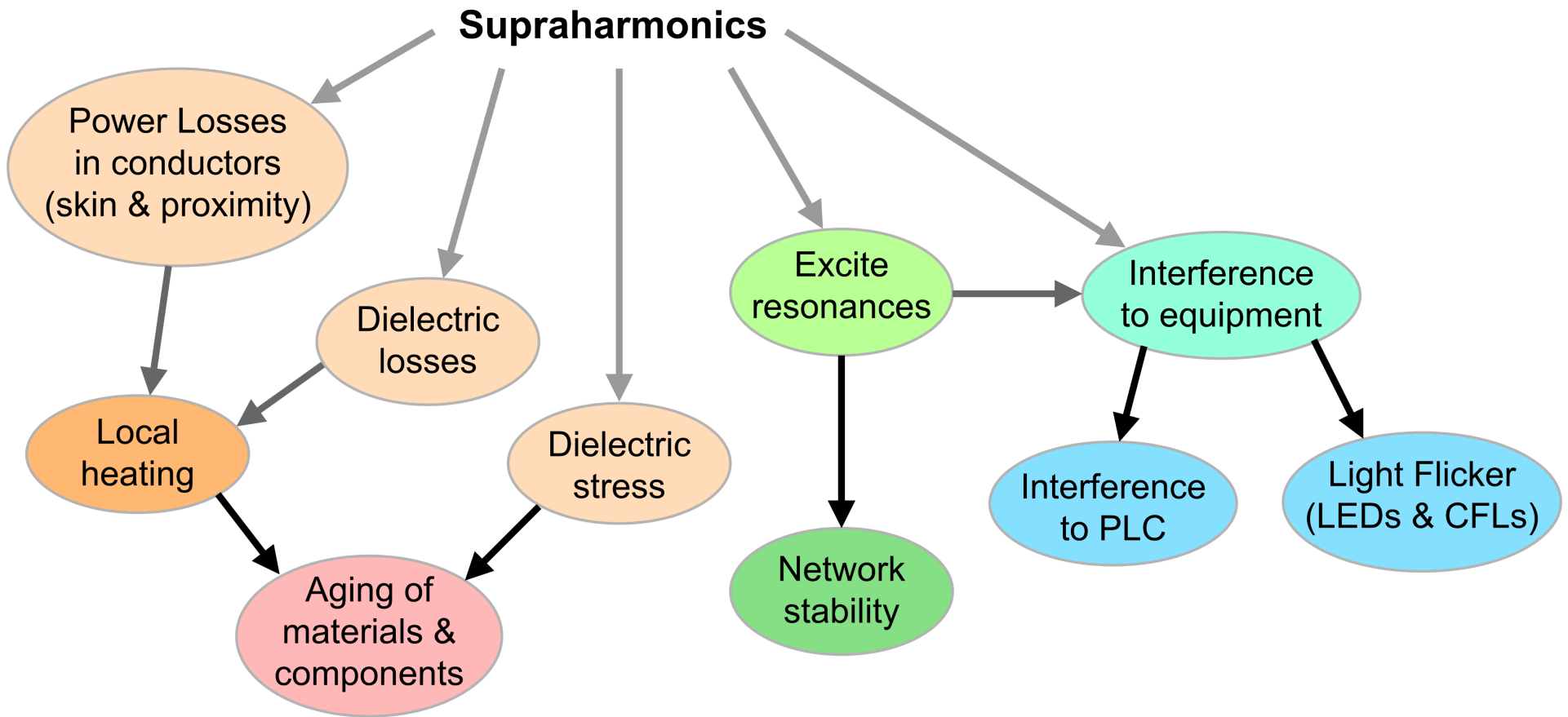


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Copper losses

Harmonic losses due to skin effect are already accounted for in normative limits

Supraharmonics (increased frequency, but reduced amplitude) add another 20% of losses



Dielectric losses

Contribution to Partial Discharges

- Quicker degradation of the material
- Both localized large electric field intensity and larger rate of change of the electric field (derivative term) matter

Self heating of dielectrics

- Non-linear phenomena take place in the wide SH range, accelerating ageing and requiring increased margin on the designed working voltage for cables (in terms of kV/mm)

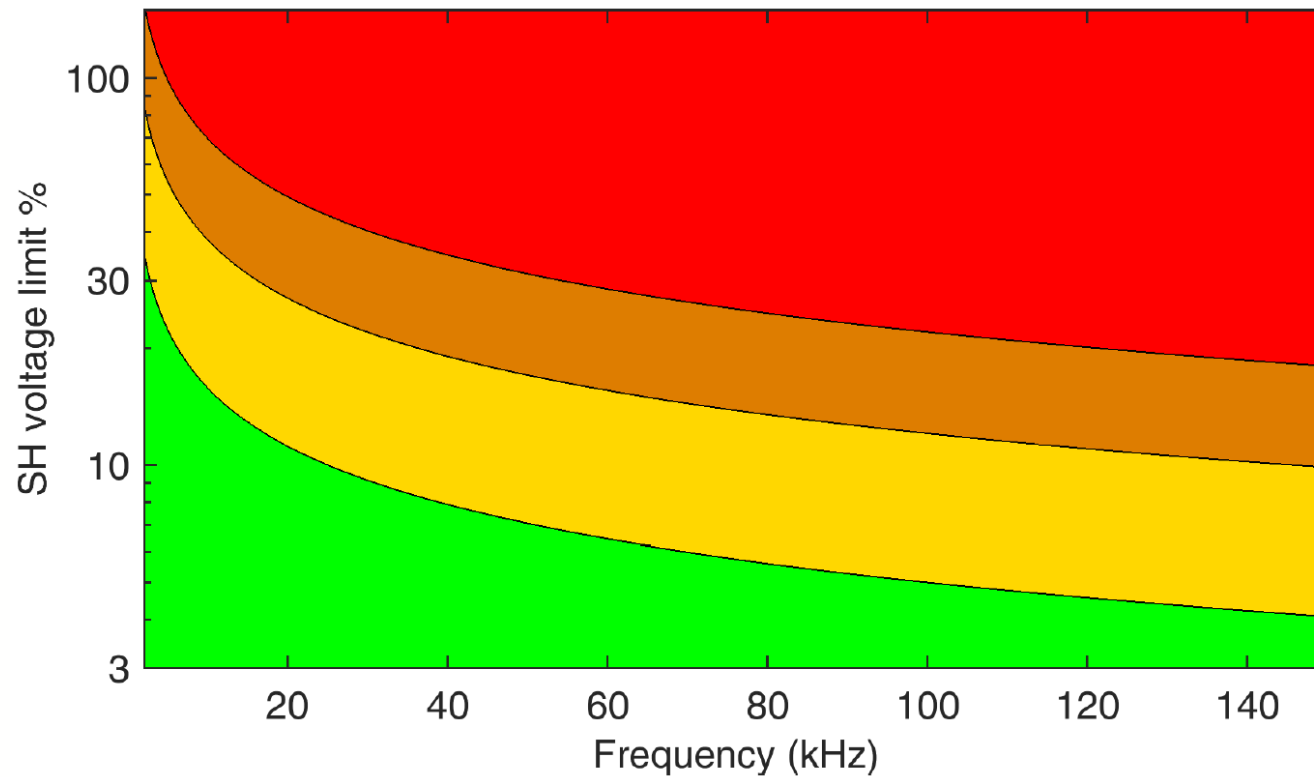
Ageing of capacitors

- Supraharmonics cause increased heating (dielectric losses)
- Capacitors wear is relevant due to secondary emissions (exchange of large SH current between adjacent equipment).



Deterioration of MV cable joints

- Local heat Q_{pu} is proportional to: $Q_{pu} = \frac{f_{sh} V_{sh}^2}{f_1 V_1^2}$
 - SH distortion intensity (square) and frequency (linear);
 - $Q_{pu} = 20$ is considered critical leading to likely failure



Green = no risk

Yellow = moderate risk

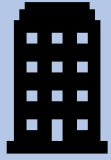
Orange = significant risk

Red = unacceptable

Figure 6. Limit curves for the percent SH voltage distortion based on the assumed $Q_{lim} = 20$ of [20] and for m values covering $m \leq 0.25$, $0.25 < m \leq 0.5$, $0.5 < m \leq 1.0$, and $m > 1.0$, with meaning of colors as in [20], namely “no risk”, “moderate risk”, “significant risk”, and “unacceptable”.

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Location



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2nd Workshop - 16th January 2025

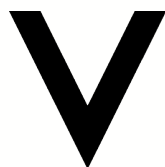


MT/BT Cabin of EV HUB



Power: 630 kVA
 $V_s = 400V$
 $V_p = 23kV$
 $I_s = 909A$
 $I_p = 15A$

Power: 400 kVA
 $V_s = 400V$
 $V_p = 23kV$
 $I_s = 577.4A$
 $I_p = 10.04A$

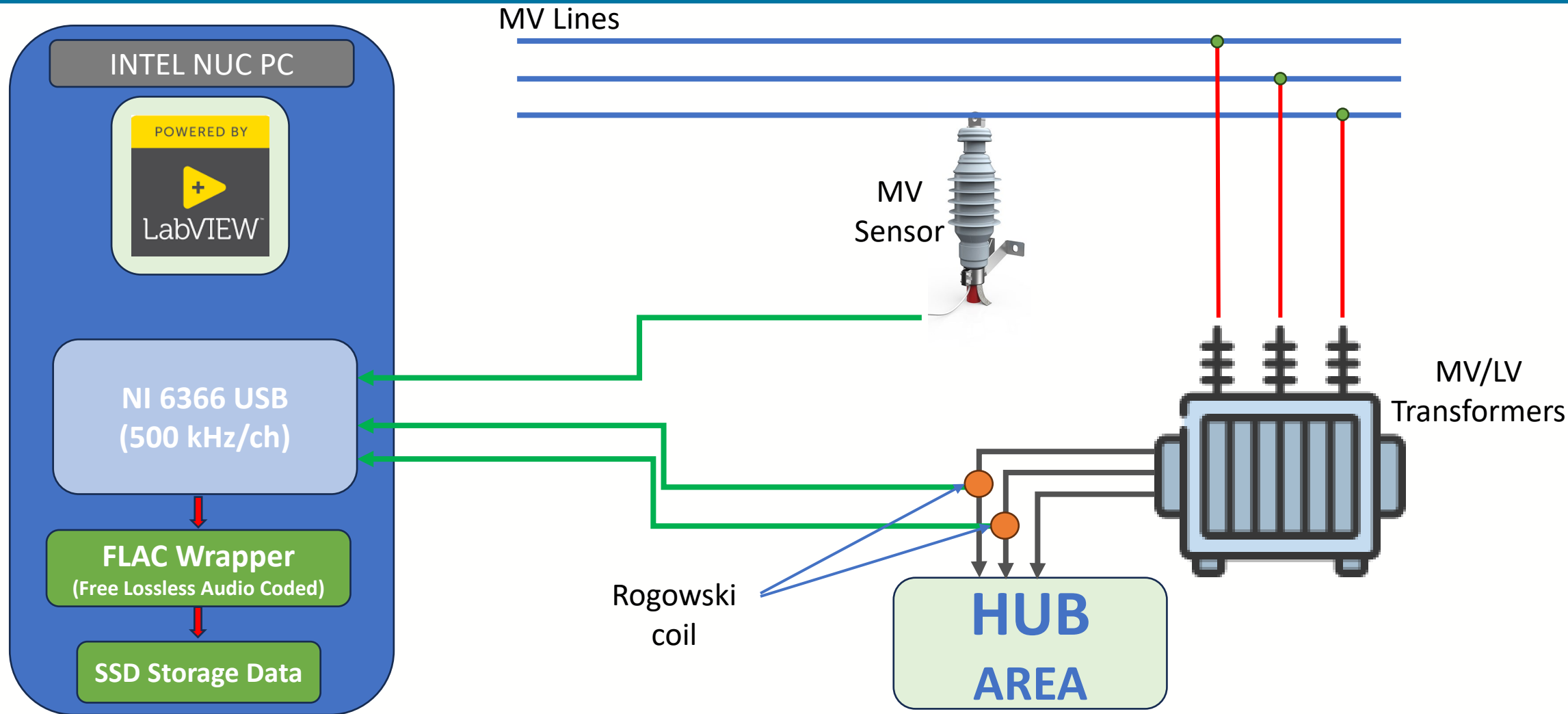


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The **VS-24-I** is a MV electronic voltage transformer for Indoor use. Its main electrical and mechanical characteristics are listed in the table below.

* marks the parameters customizable upon request.

Rated insulation level	24/50/125 kV
Accuracy class *	0.5
Rated primary voltage, U_{pn} *	$20/\sqrt{3}$ kV
Maximum voltage, U_m	24 kV
Rated secondary voltage, U_{sn} *	1 V
Rated voltage factor, K_u	1.9 for 8h
Nominal frequency	50 / 60 Hz
Nominal transformation ratio, K_n *	$20/\sqrt{3}$ kV / 1 V
Auxiliary Supply voltage	± 12 Vdc
Max. Supply current	15 mA
Creepage	375 mm
Primary terminal capacity	1 pF
Bandwidth (-1 dB)	30 Hz – 20 kHz, 1 MHz for HF version
Applicable Standards	IEC 60044-7, IEC 60660
Accuracy on harmonics	According to IEC 60044-8
Weight	1.6 kg
Temperature range	[- 5 °C, 40 °C]



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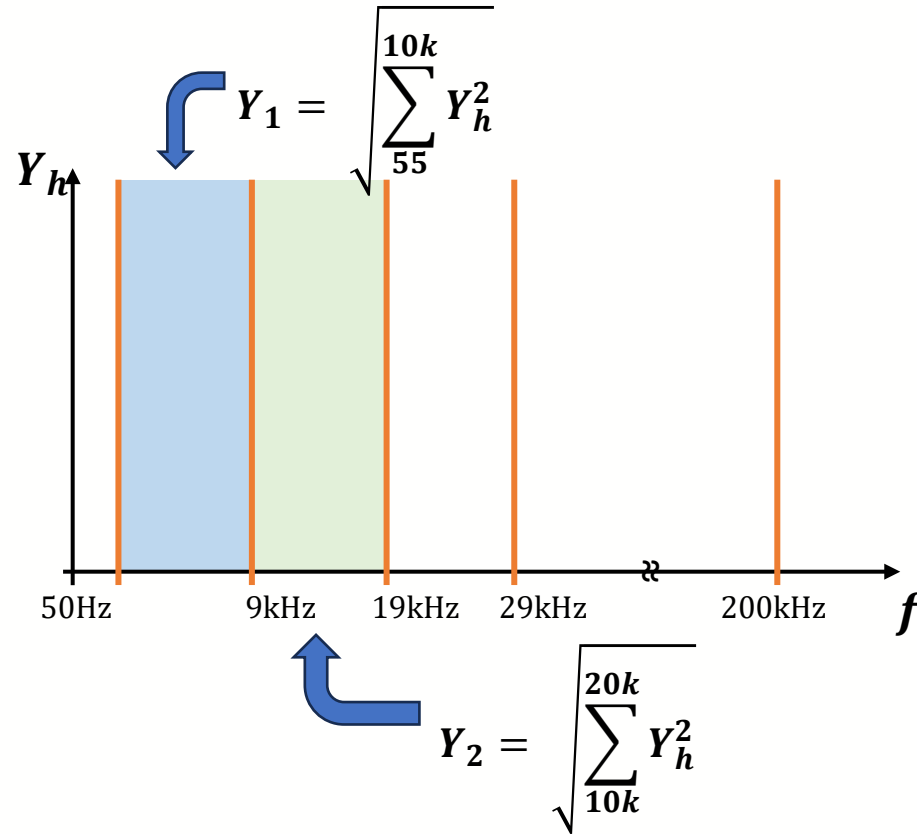
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Measurement indices



Band Group

$$Y_g = \sqrt{\sum_{f_a}^{f_b} Y_h^2} \rightarrow \begin{cases} Y_{g_{max}} \\ Y_{g_{mean}} \\ Y_{g_{min}} \end{cases}$$

Where $|f_b - f_a| = 10 \text{ kHz}$

FFT \rightarrow Y_h **Window Size**
200 ms



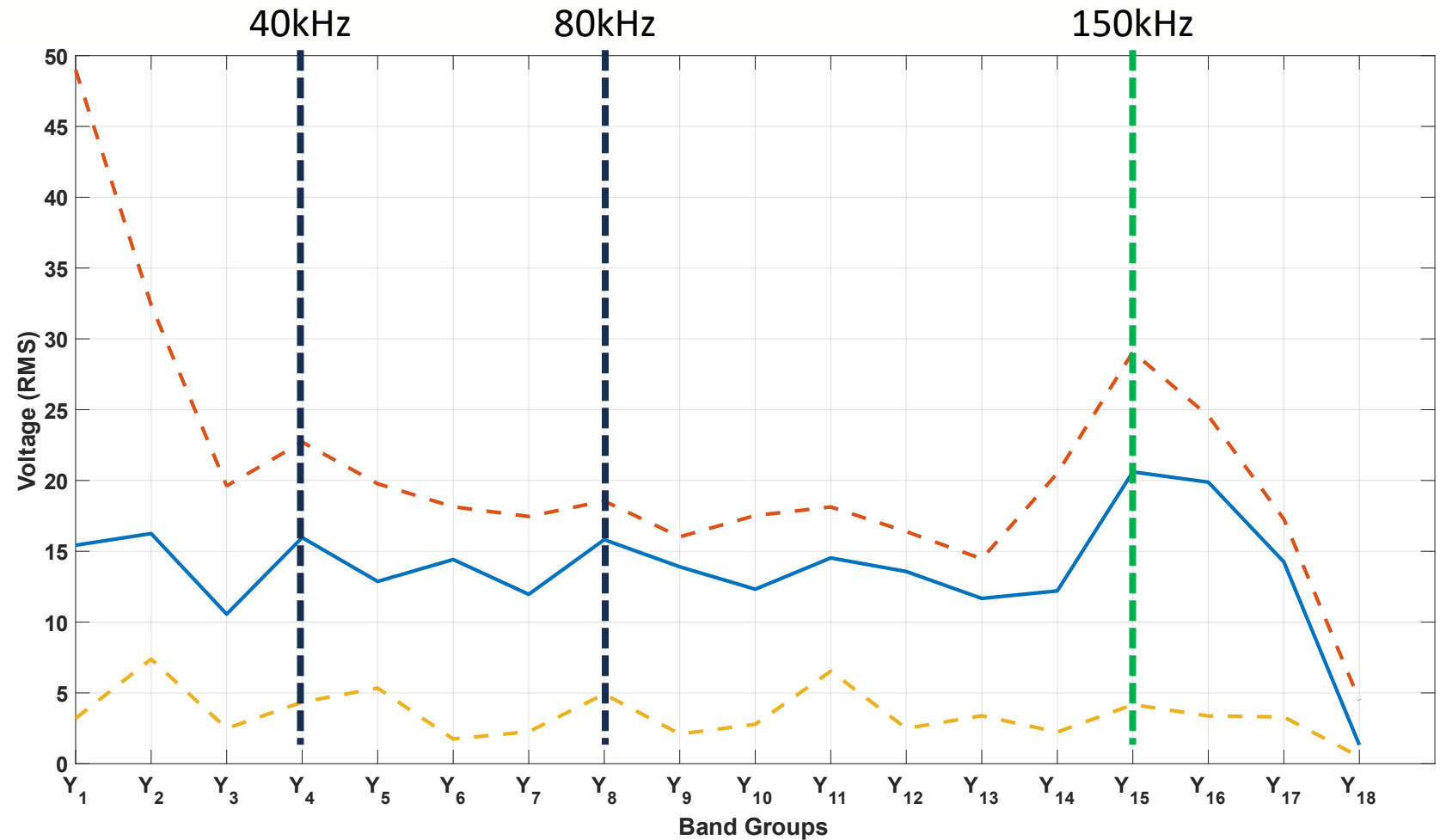
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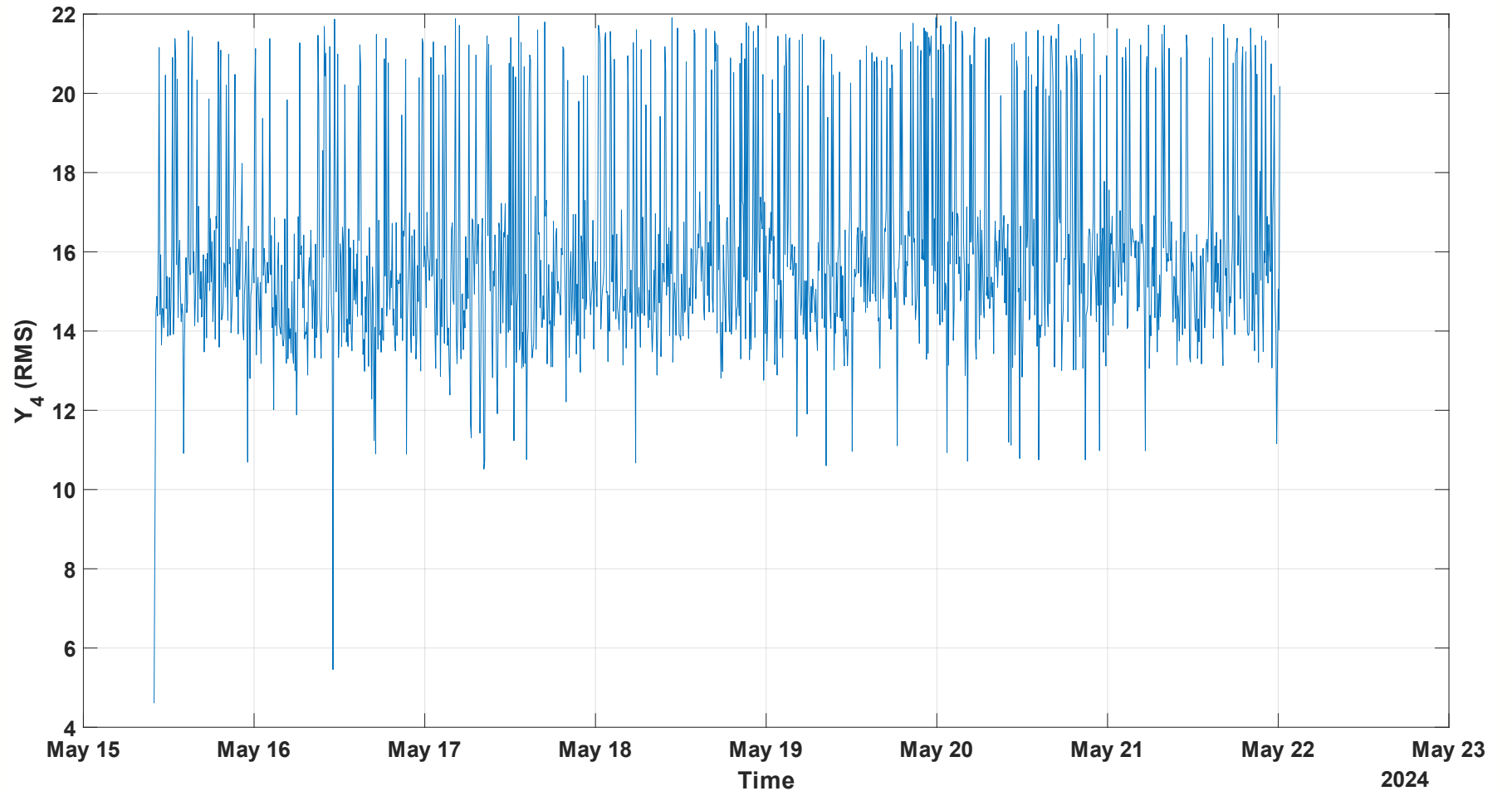


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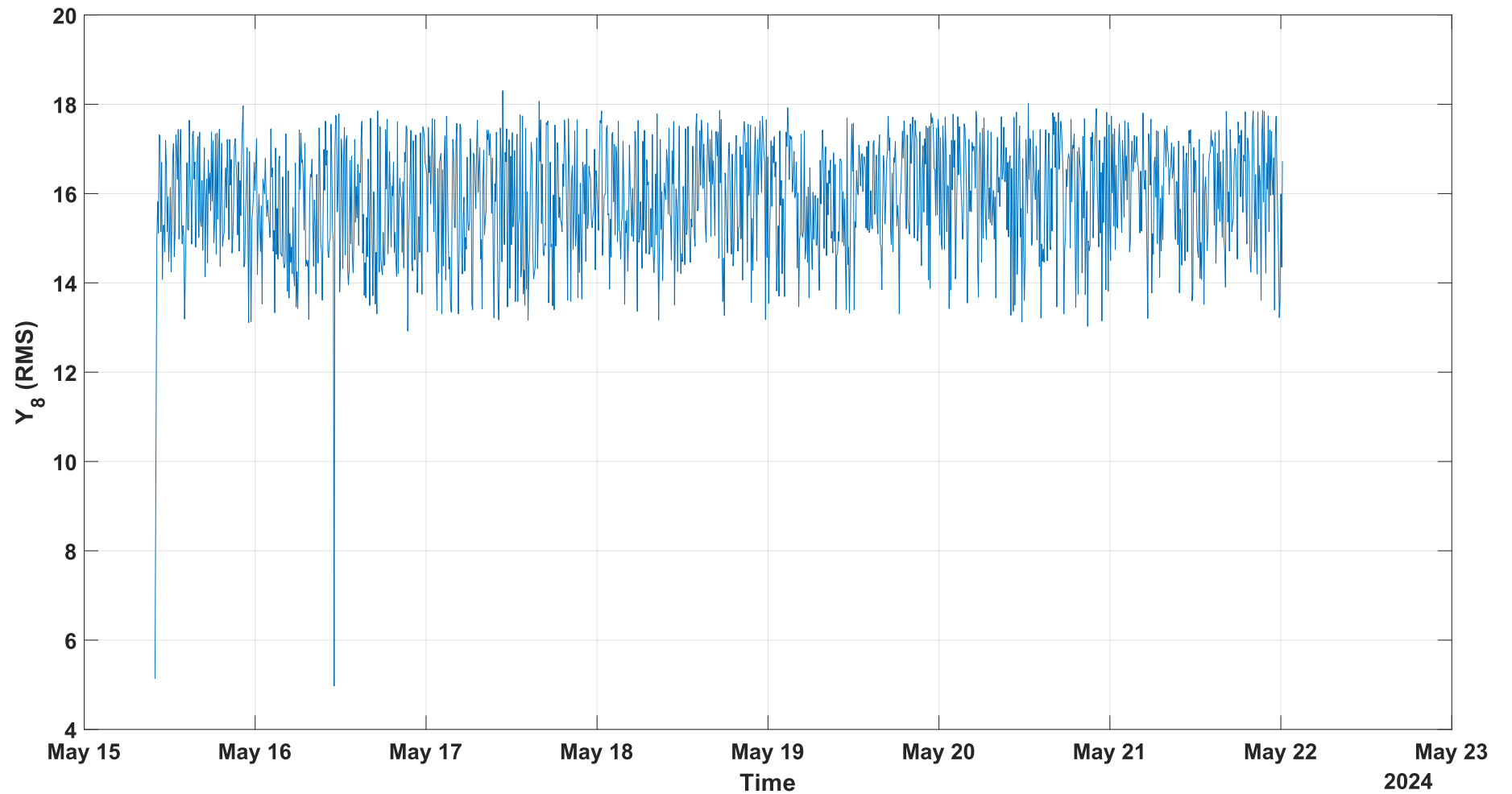
Fundamental voltage
 $V_1 = 15 \text{ kV (RMS)}$



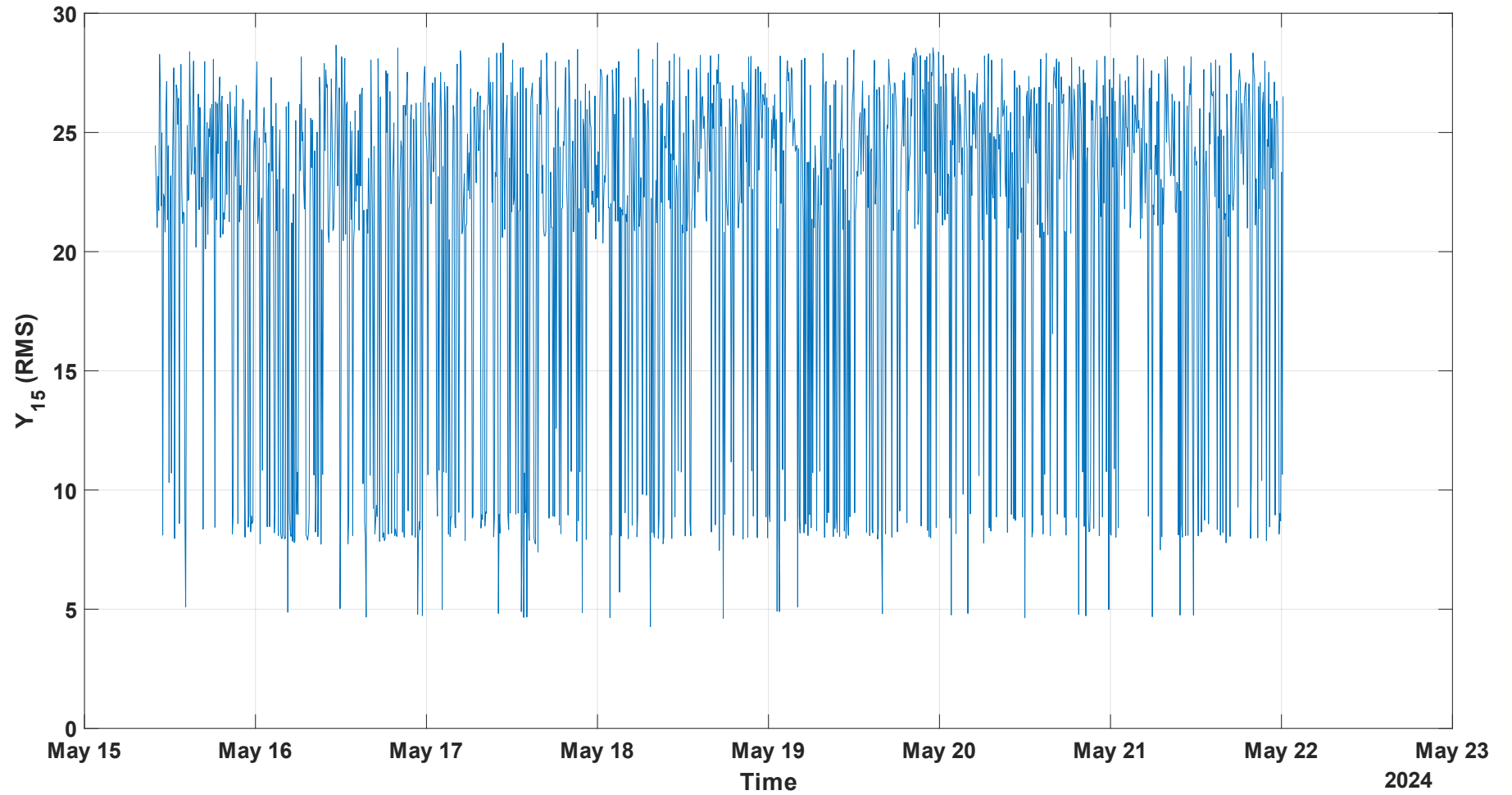
$$Y_4 = \sqrt{\sum_{30k}^{40k} Y_h^2}$$



$$Y_8 = \sqrt{\sum_{70k}^{80k} Y_h^2}$$

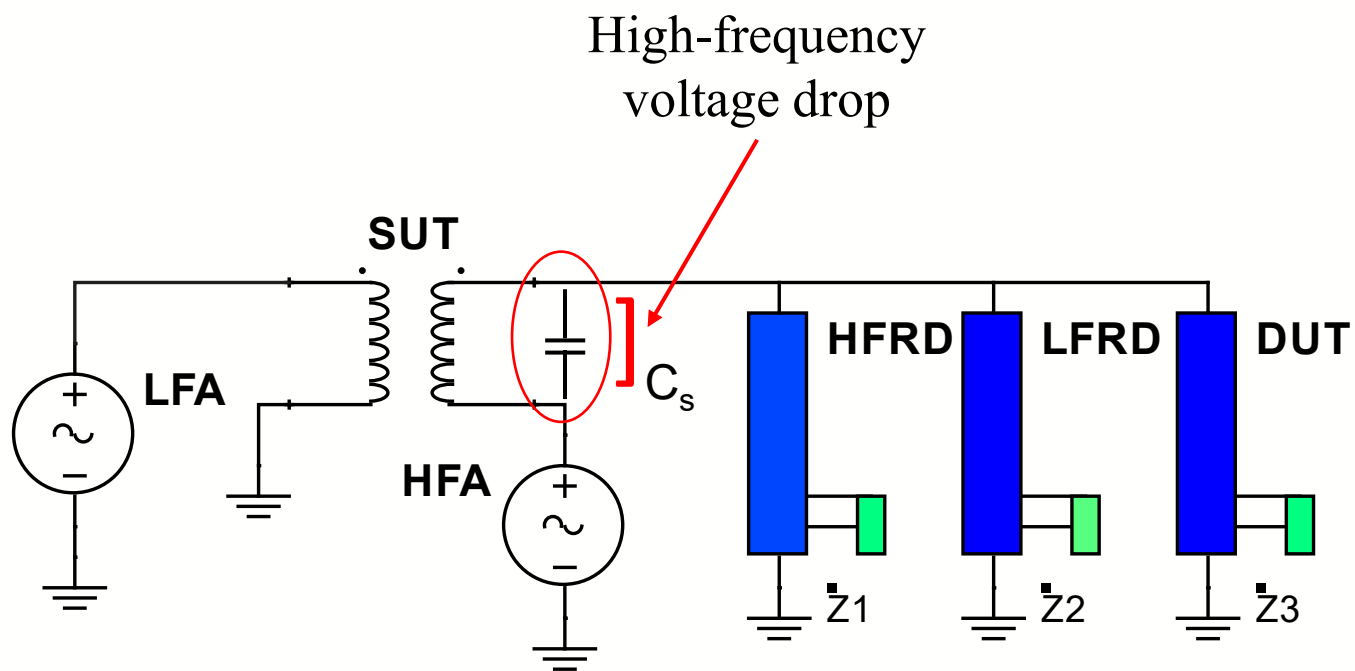


$$Y_{15} = \sqrt{\sum_{140k}^{150k} Y_h^2}$$



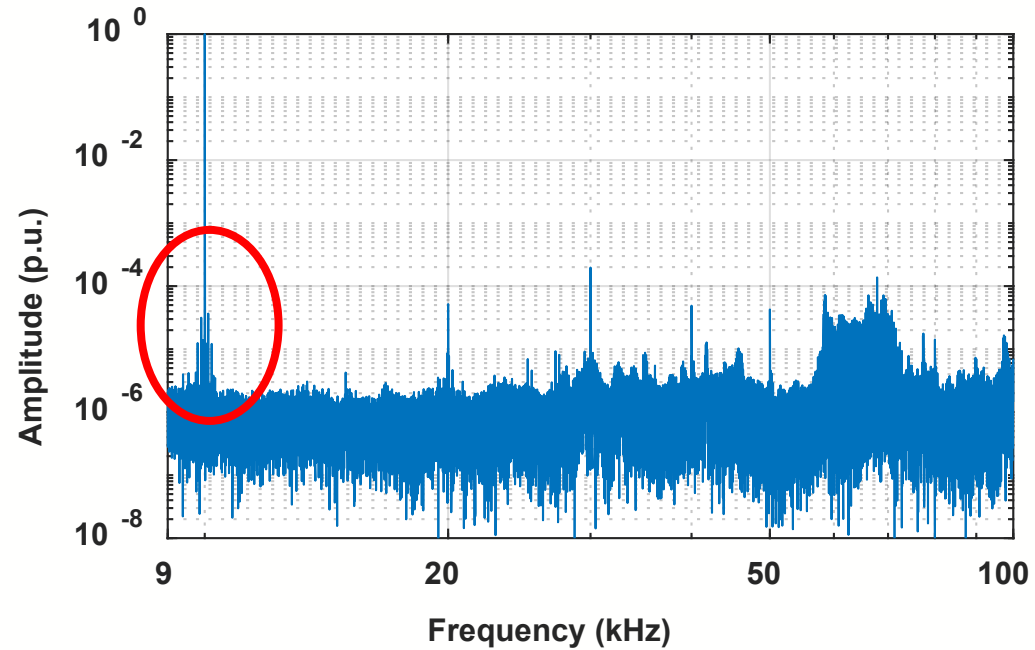
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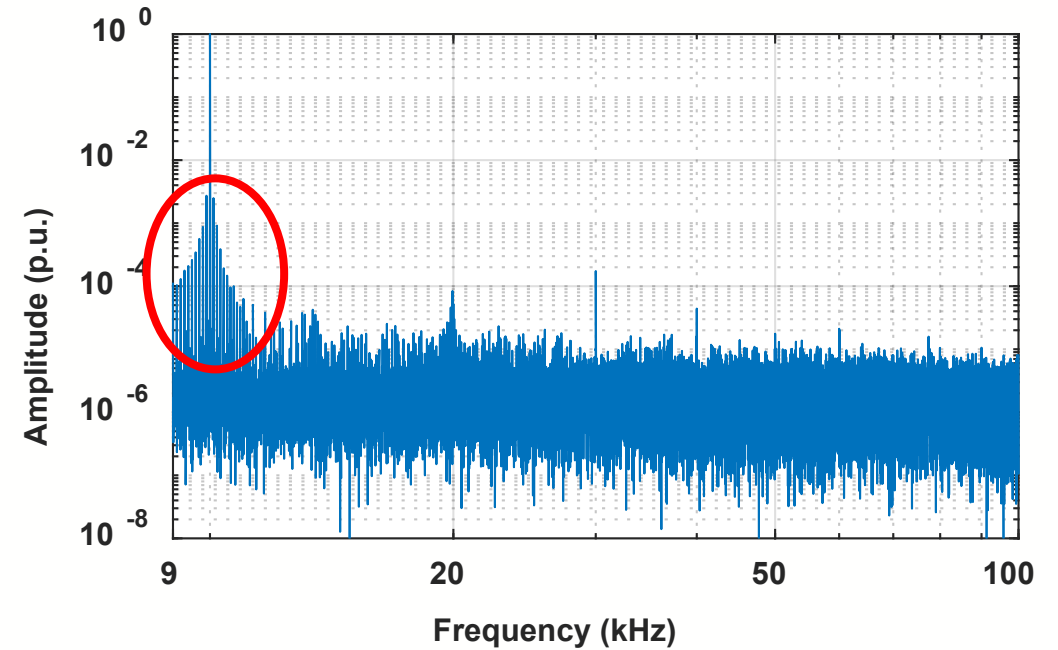


LFA	Low-Frequency Amplifier
HFA	High-Frequency Amplifier
SUT	Step-Up Transformer
LFRD	Low-Frequency Reference Device
HFRD	High-Frequency Reference Device
DUT	Device Under Test

Input spectrum ($f_{hf} = 10 \text{ kHz}$)



Output spectrum ($f_{hf} = 10 \text{ kHz}$)



More details later....

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22NRM06 ADMIT - M18 Meeting

LNE, 3 December 2024



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